



Effects of Cutting Parameters and Tool Wear in Hard Turning

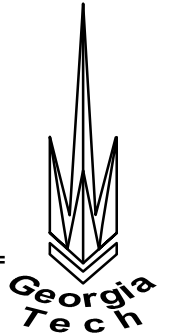
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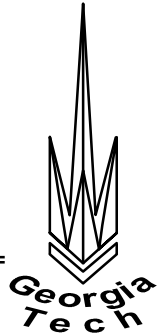
October 20th, 1999

Presentation Outline



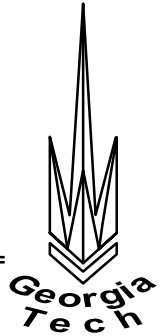
- ❖ Brief background/intro to hard turning
- ❖ Experimental results
- ❖ Conclusions and recommendations

What is hard turning?



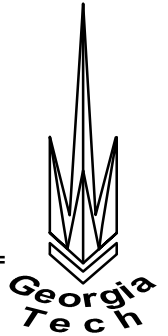
- ❖ Turning “hard” material
- ❖ “Hard” is arbitrarily defined above 45 HRC
- ❖ Some materials may be up to 70 HRC
- ❖ Typical materials
 - Heat treated steels
 - Case hardened steels
- ❖ Cutting tools
 - Carbide
 - Ceramics (Al_2O_3 and TiC)
 - Cubic Boron Nitride (CBN)

Importance of hard turning



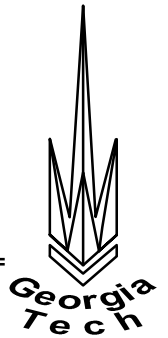
- ❖ Industry is very interested
- ❖ Hard turning may replace many grinding operations
 - Increased flexibility
 - Decreased cycle times
 - Decreased number of machine tools
 - Less expensive machine tools
 - Significantly decreased setup times
 - Environmentally friendly (dry cutting)

So why doesn't everyone hard turn?

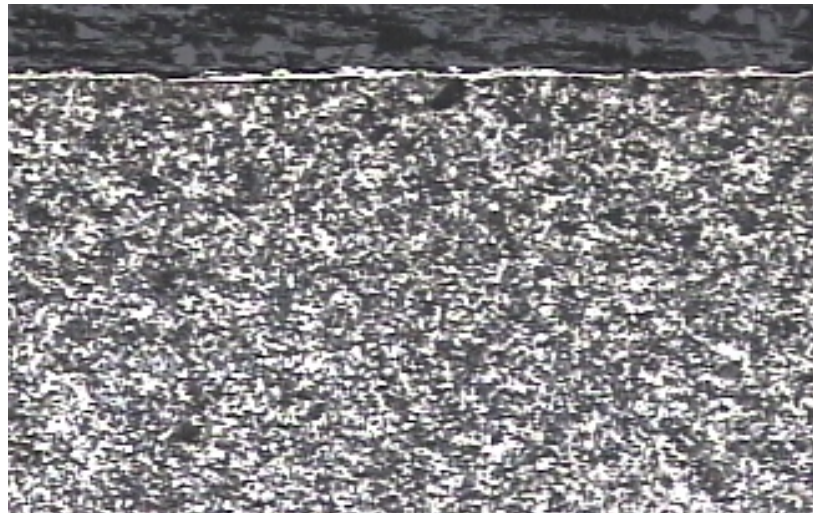


- ❖ Rigid machine tools and cutting inserts have just recently made this process feasible
- ❖ Advantages of “centerless” grinding are still significant
- ❖ Tool costs can be expensive if tool life is short
- ❖ Surface finish and geometry is still questionable
- ❖ Surface integrity has been a problem

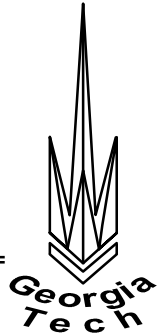
Research Objective



- ❖ Determine the effect of varying cutting conditions
 - cutting forces
 - tool wear
 - “white layer”
 - surface finish

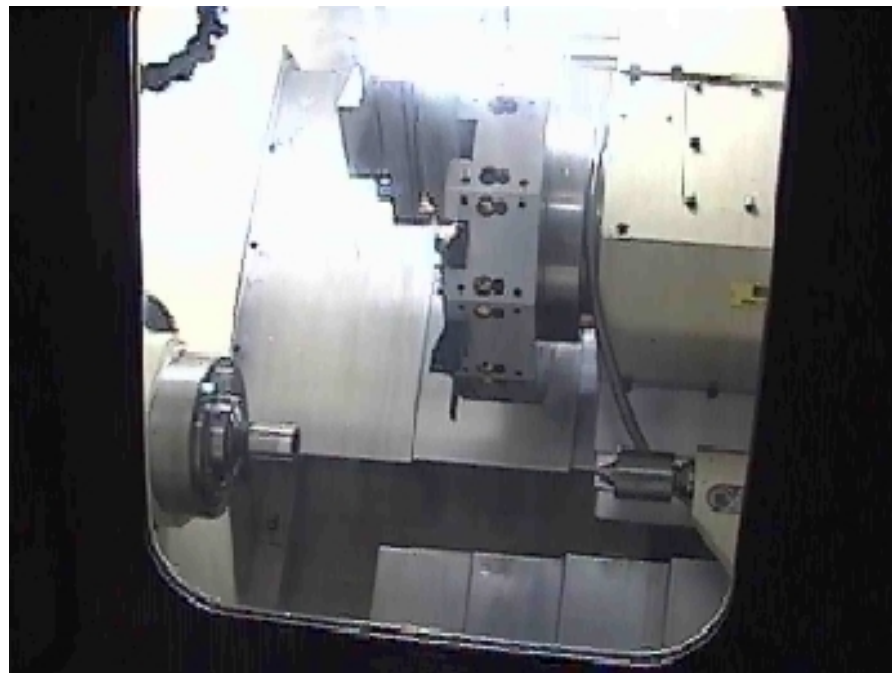
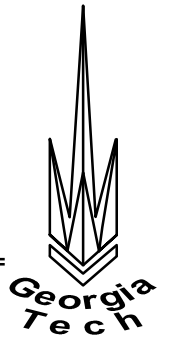


Test Conditions

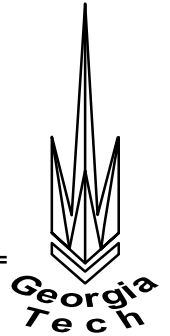


Cutting condition	Radial depth of cut	Cutting speed	Feed rate
1	0.203 mm	182.9 m/min	0.152 mm/rev
2	0.203 mm	91.4 m/min	0.076 mm/rev
3	0.203 mm	91.4 m/min	0.076 mm/rev
4	0.203 mm	182.9 m/min	0.152 mm/rev
5	0.508 mm	182.9 m/min	0.152 mm/rev
6	0.203 mm	182.9 m/min	0.152 mm/rev
1	0.008 in	600 ft/min	0.006 in/rev
2	0.008 in	300 ft/min	0.003 in/rev
3	0.008 in	300 ft/min	0.006 in/rev
4	0.008 in	600 ft/min	0.003 in/rev
5	0.020 in	600 ft/min	0.006 in/rev
6	0.008 in	600 ft/min	0.006 in/rev

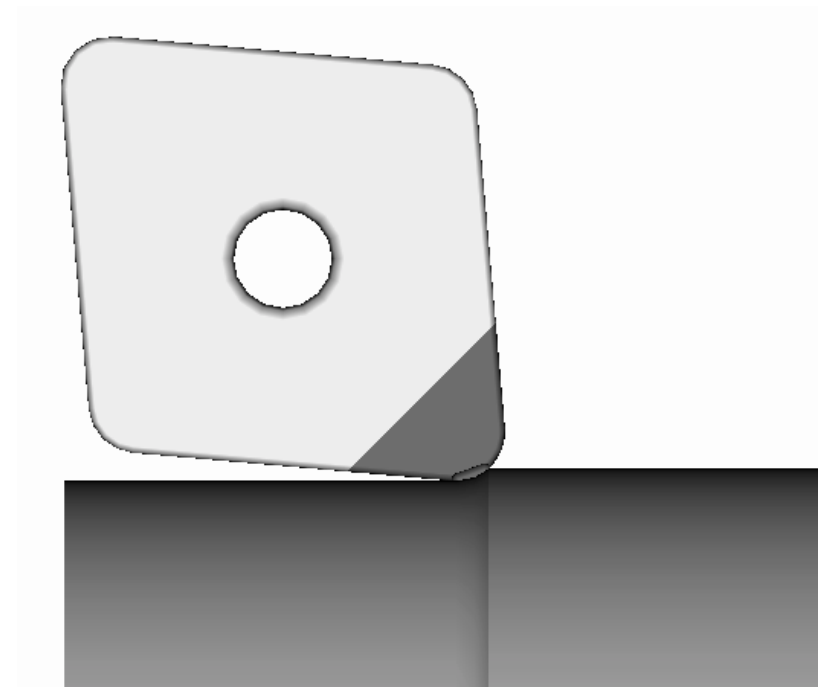
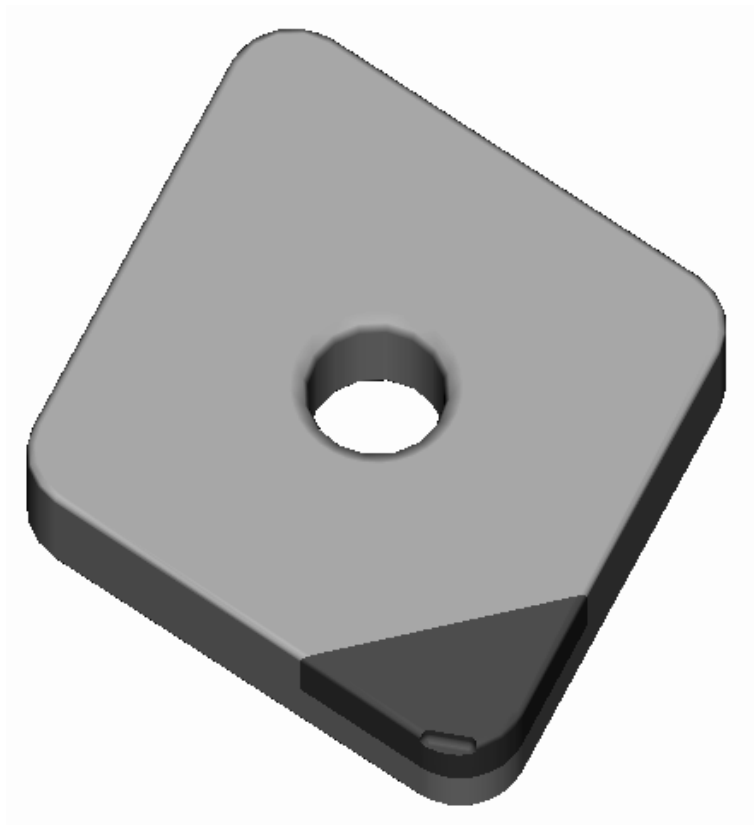
Experimental Demonstration



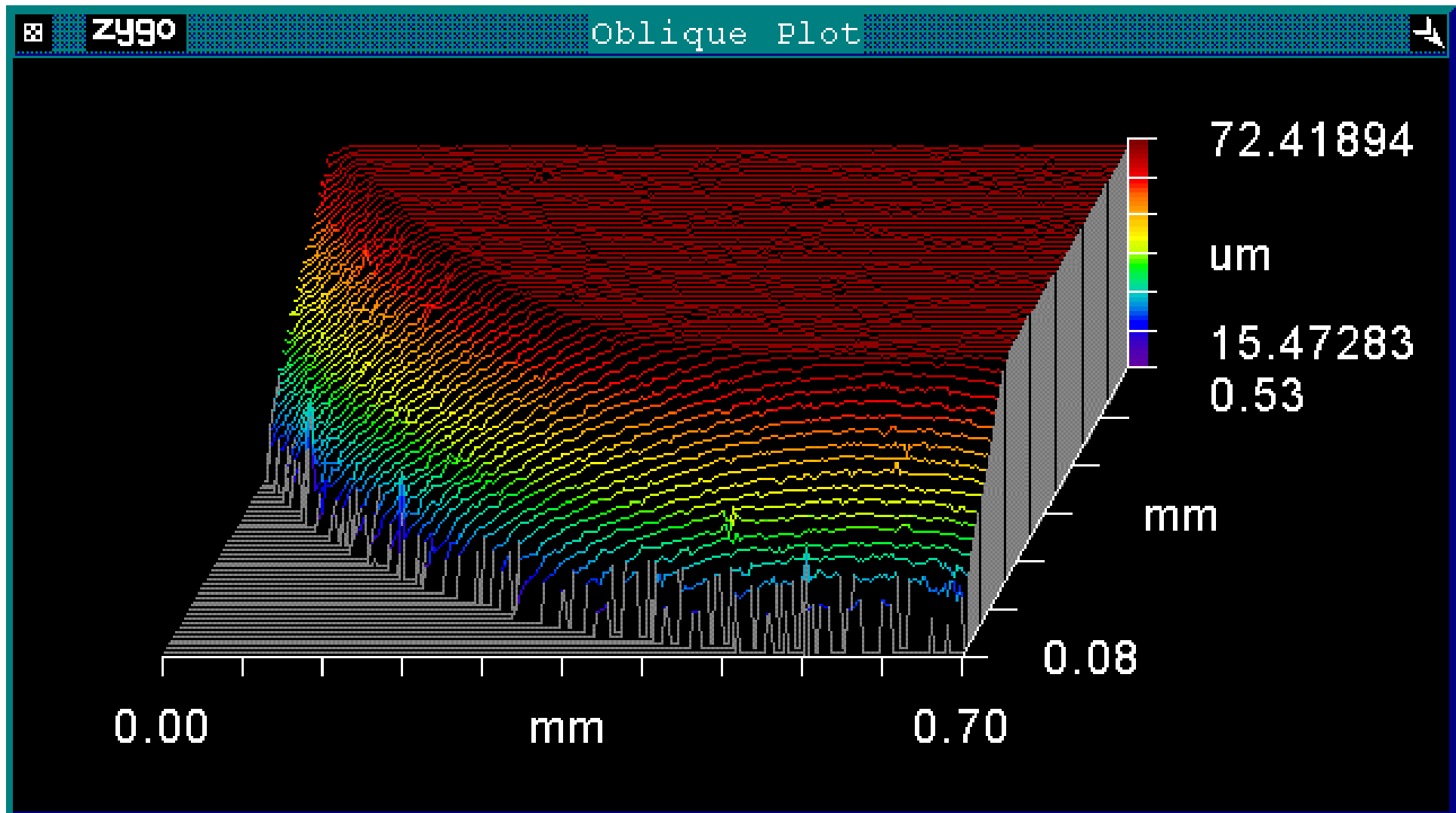
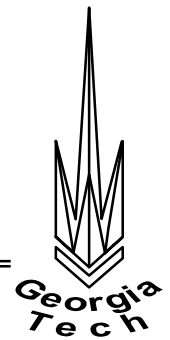
Tool Wear Results



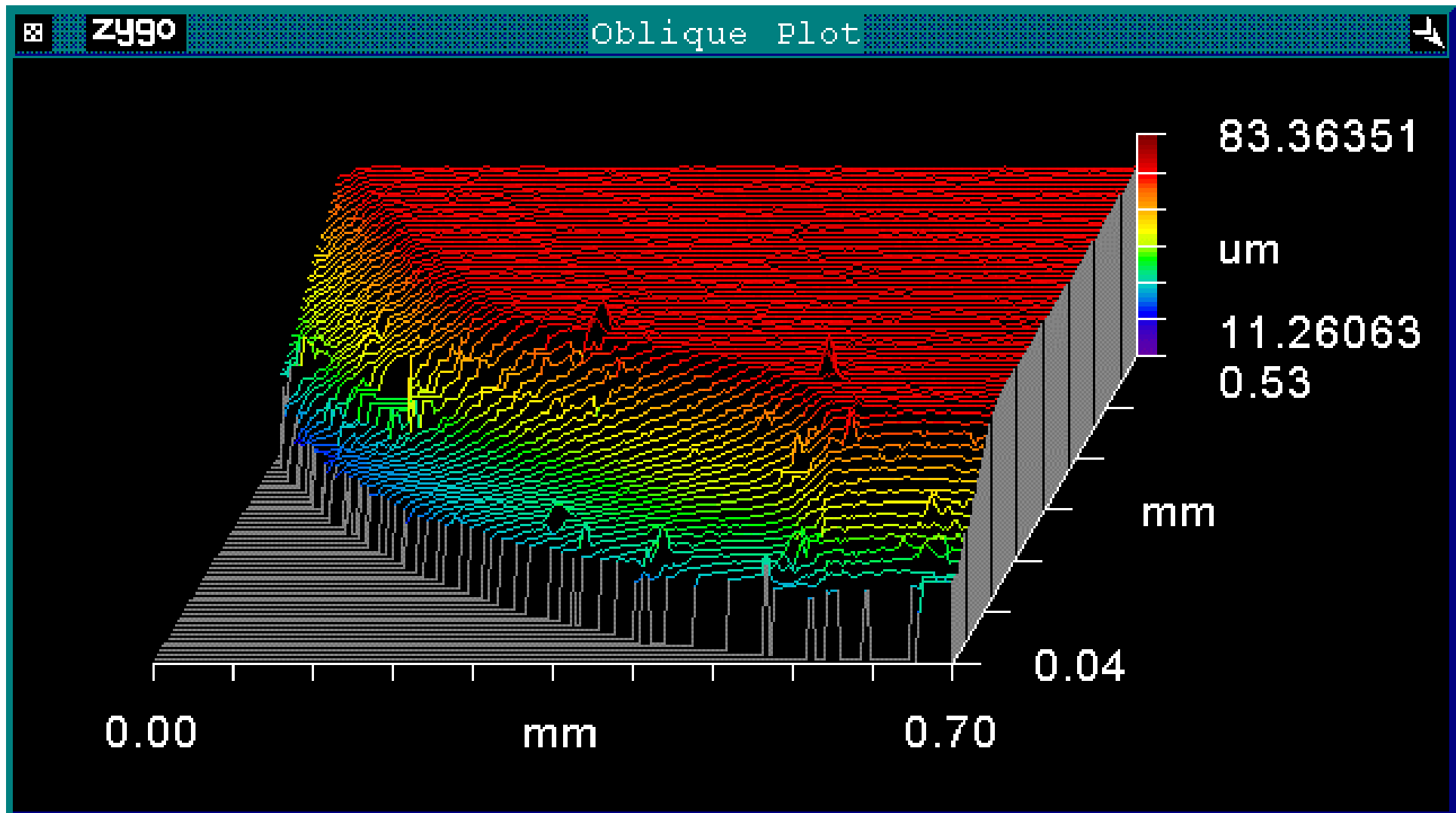
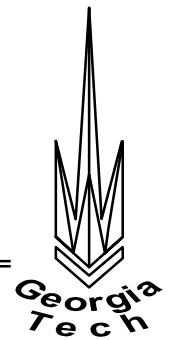
- ❖ Tool wear occurs on nose radius of the tool
- ❖ At a 0.203mm (0.008") depth of cut, the cut also occurs primarily on the 20° chamfer



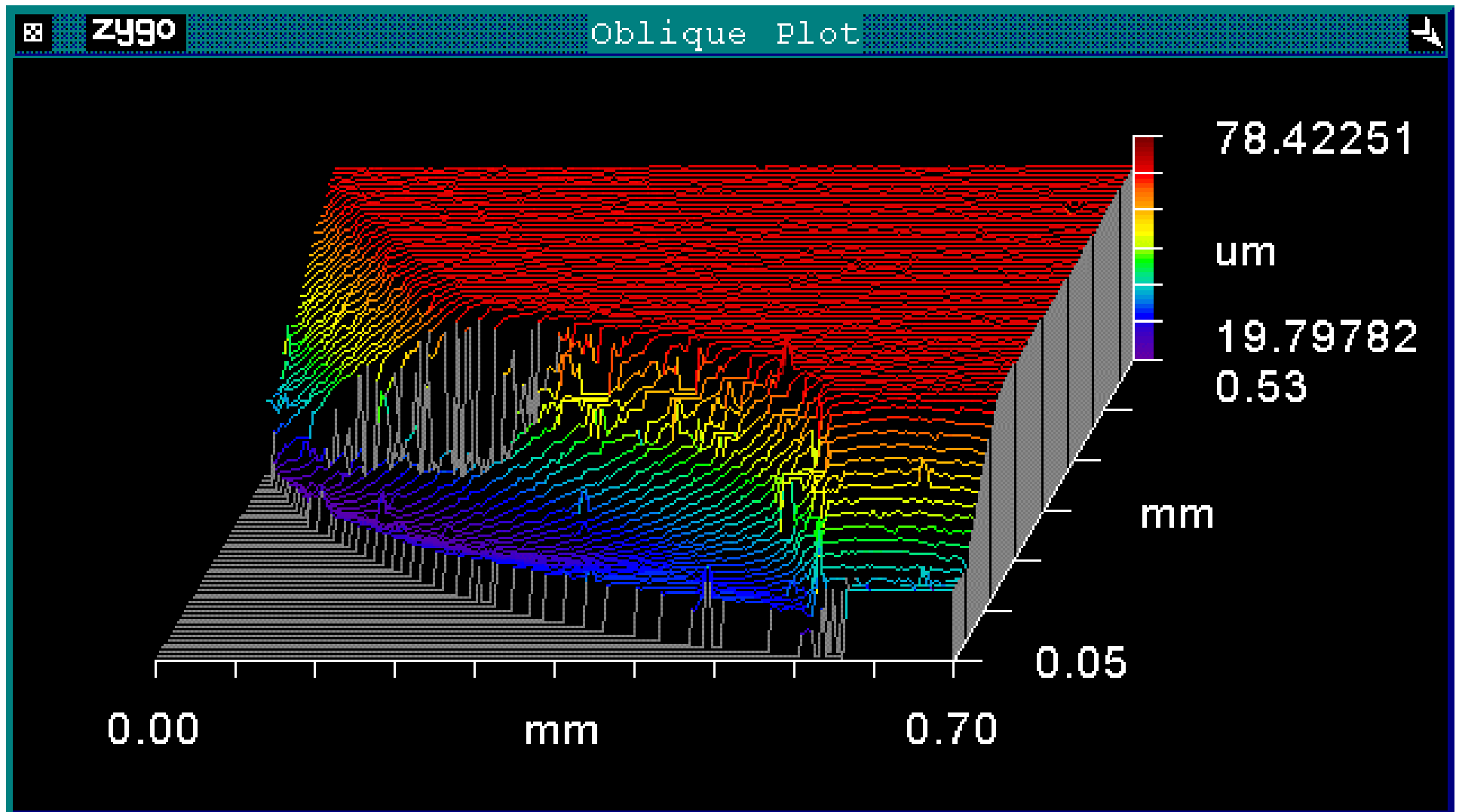
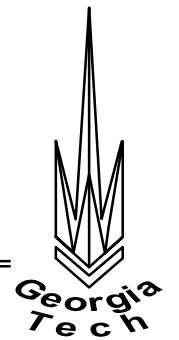
Progression of Crater Wear



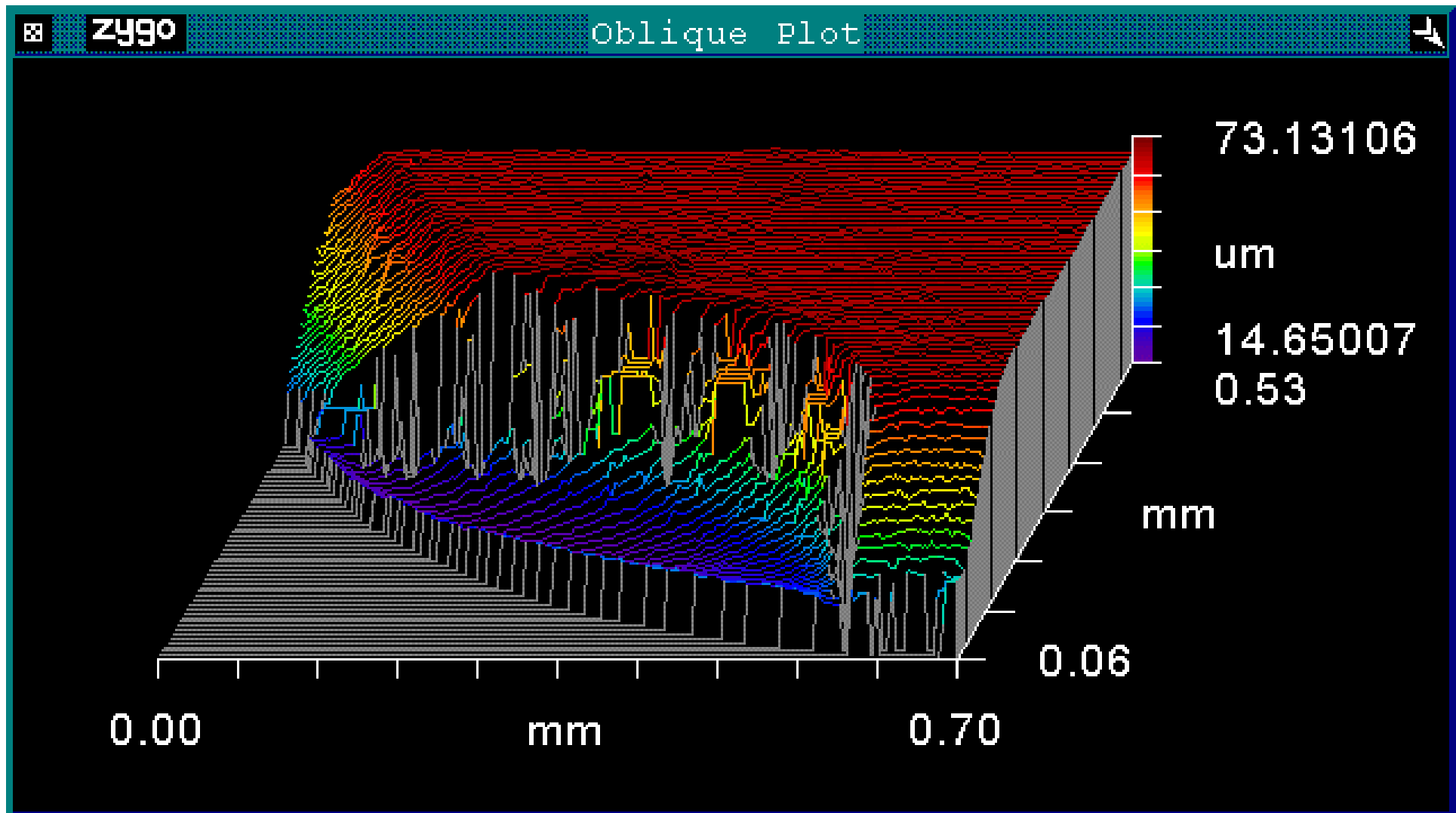
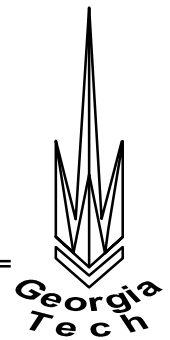
Progression of Crater Wear



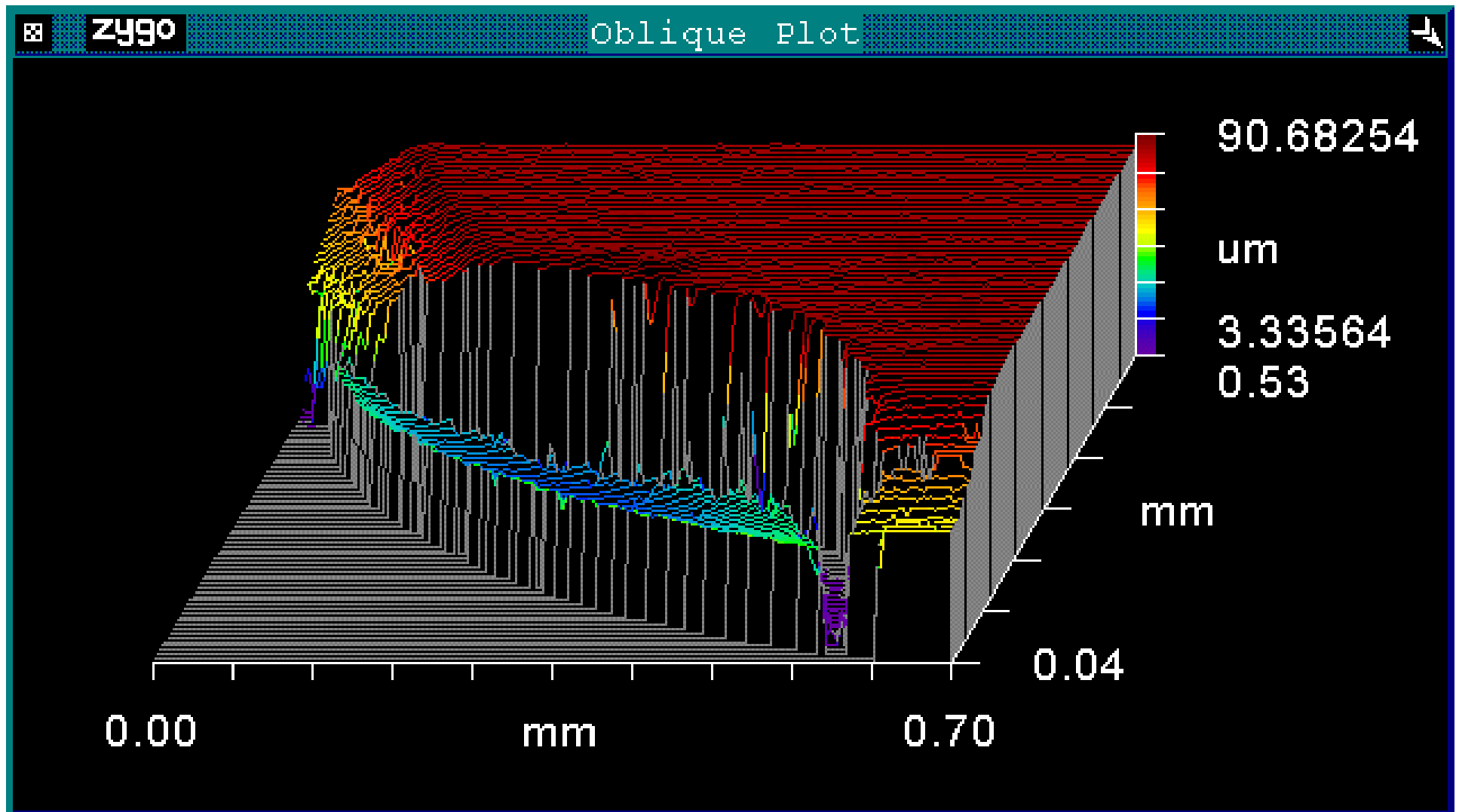
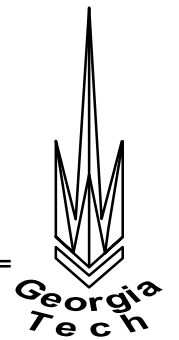
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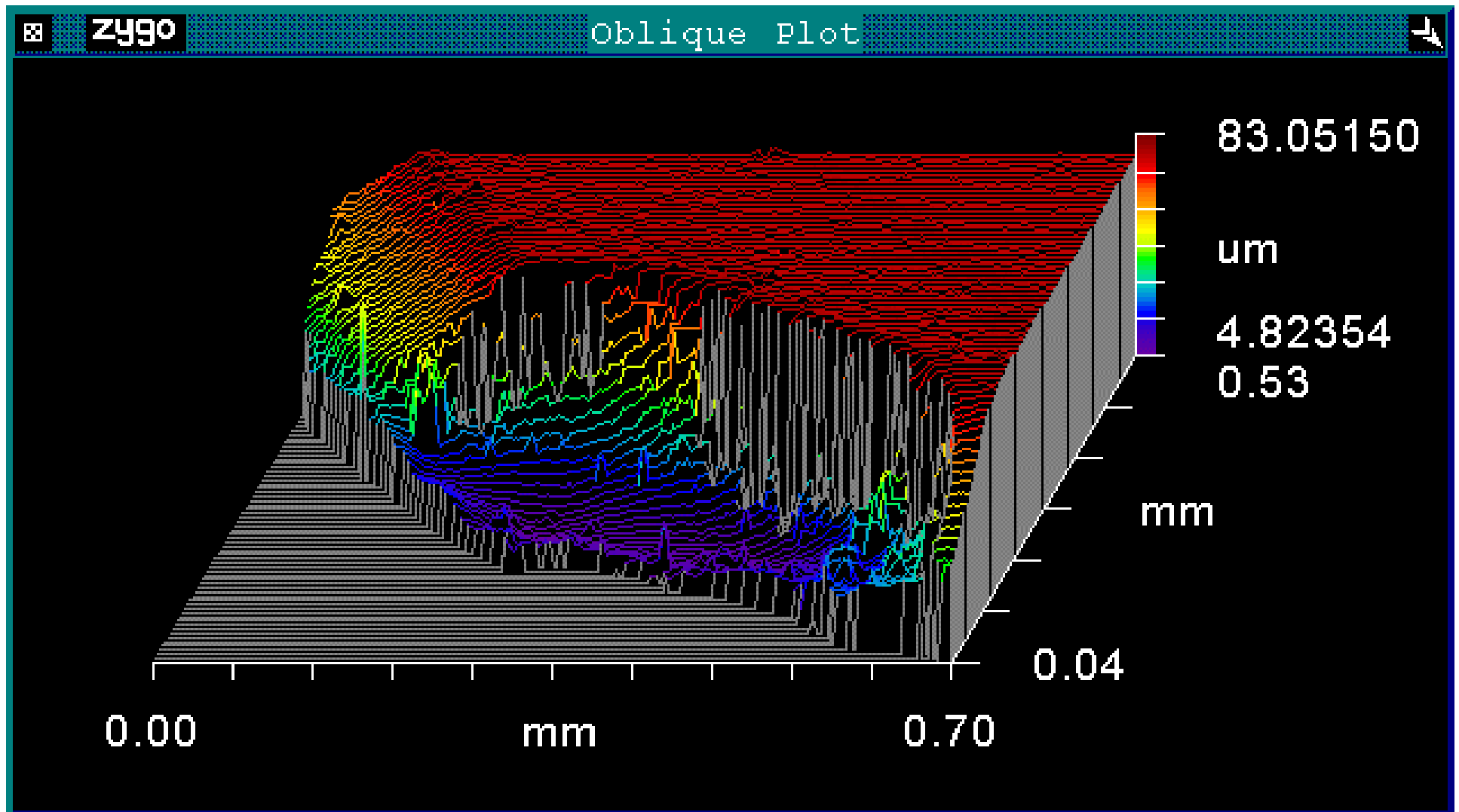
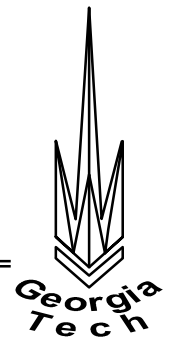
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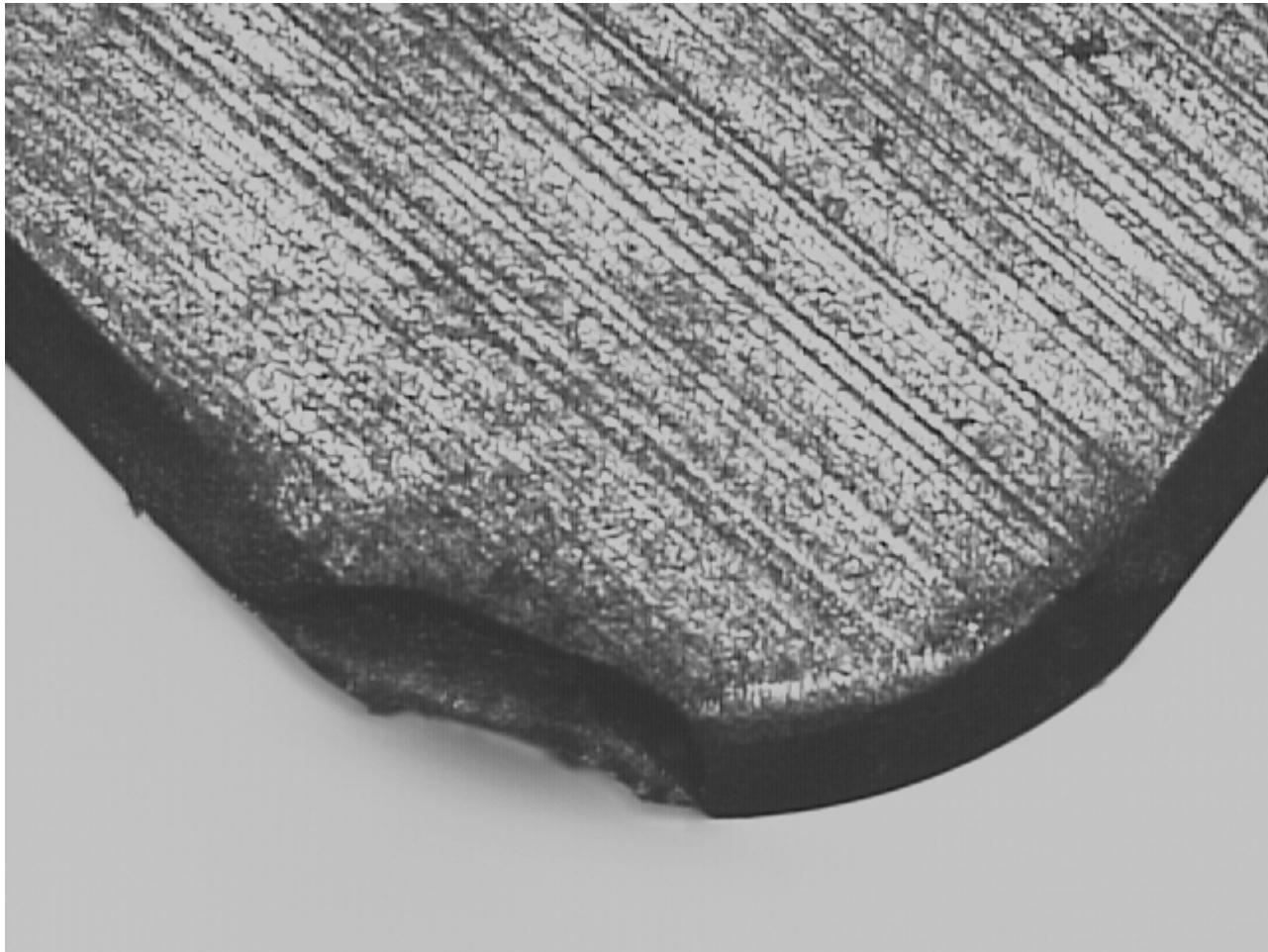
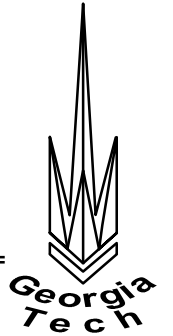
Progression of Crater Wear



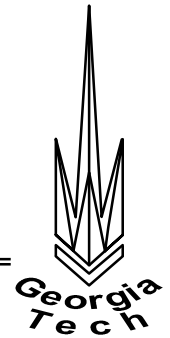
Progression of Crater Wear



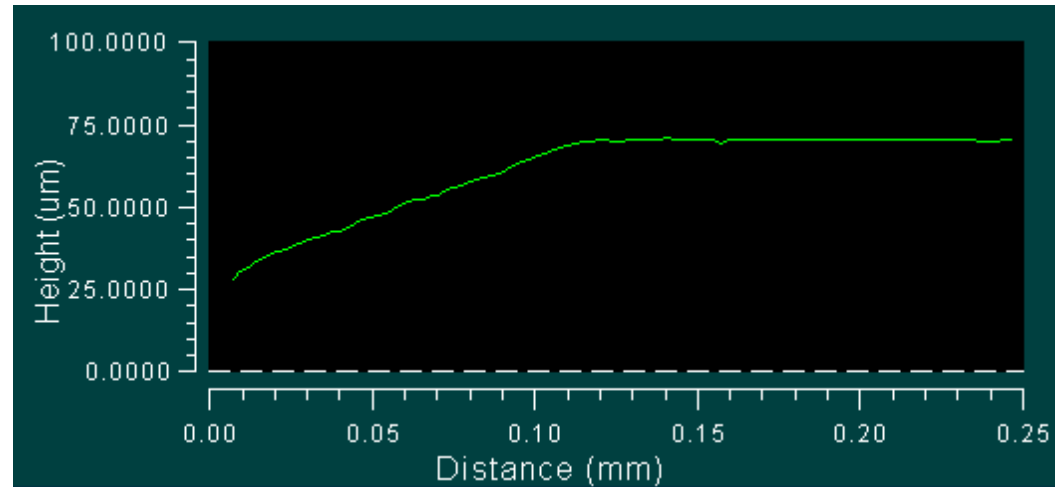
Tool Failure



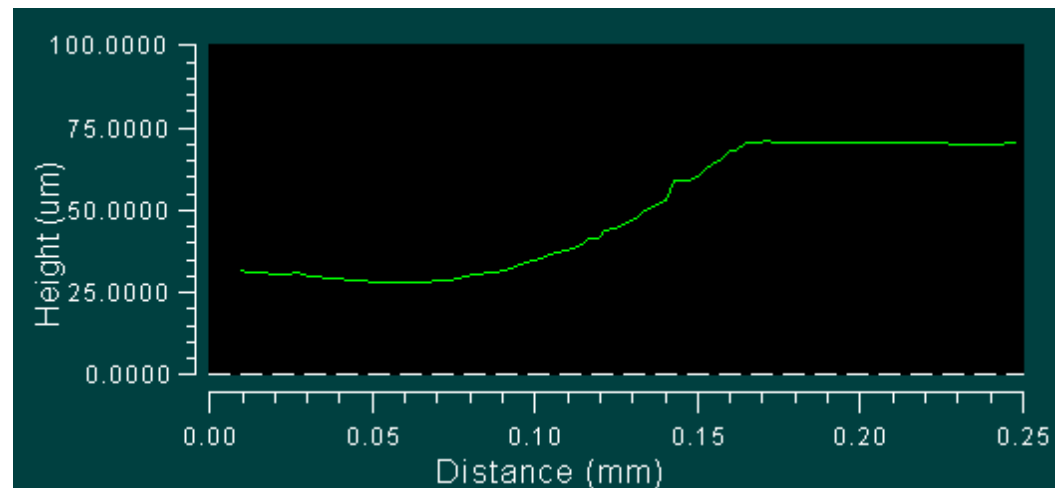
Changes in Cutting Edge Geometry



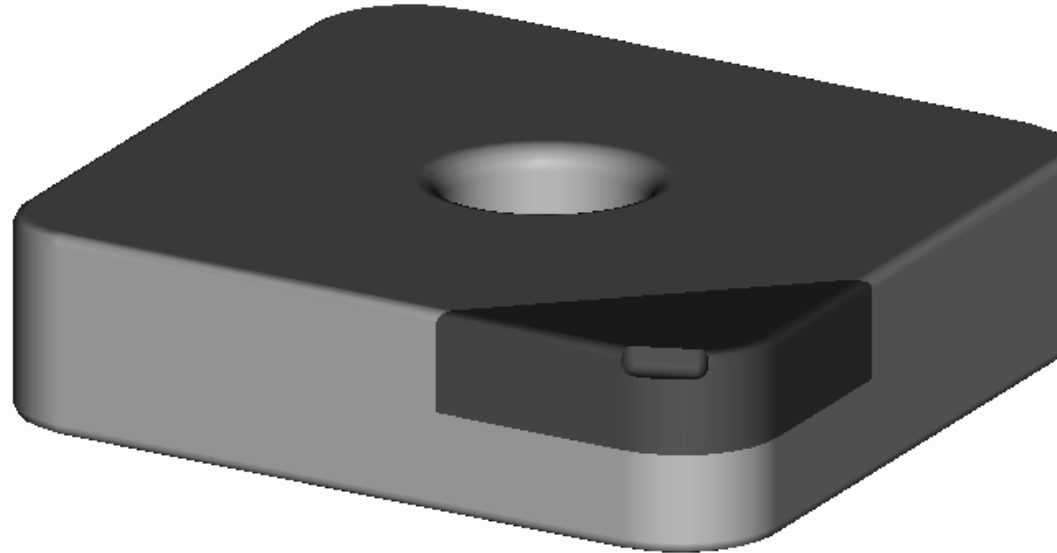
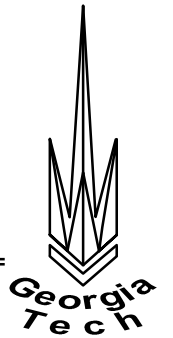
New Tool



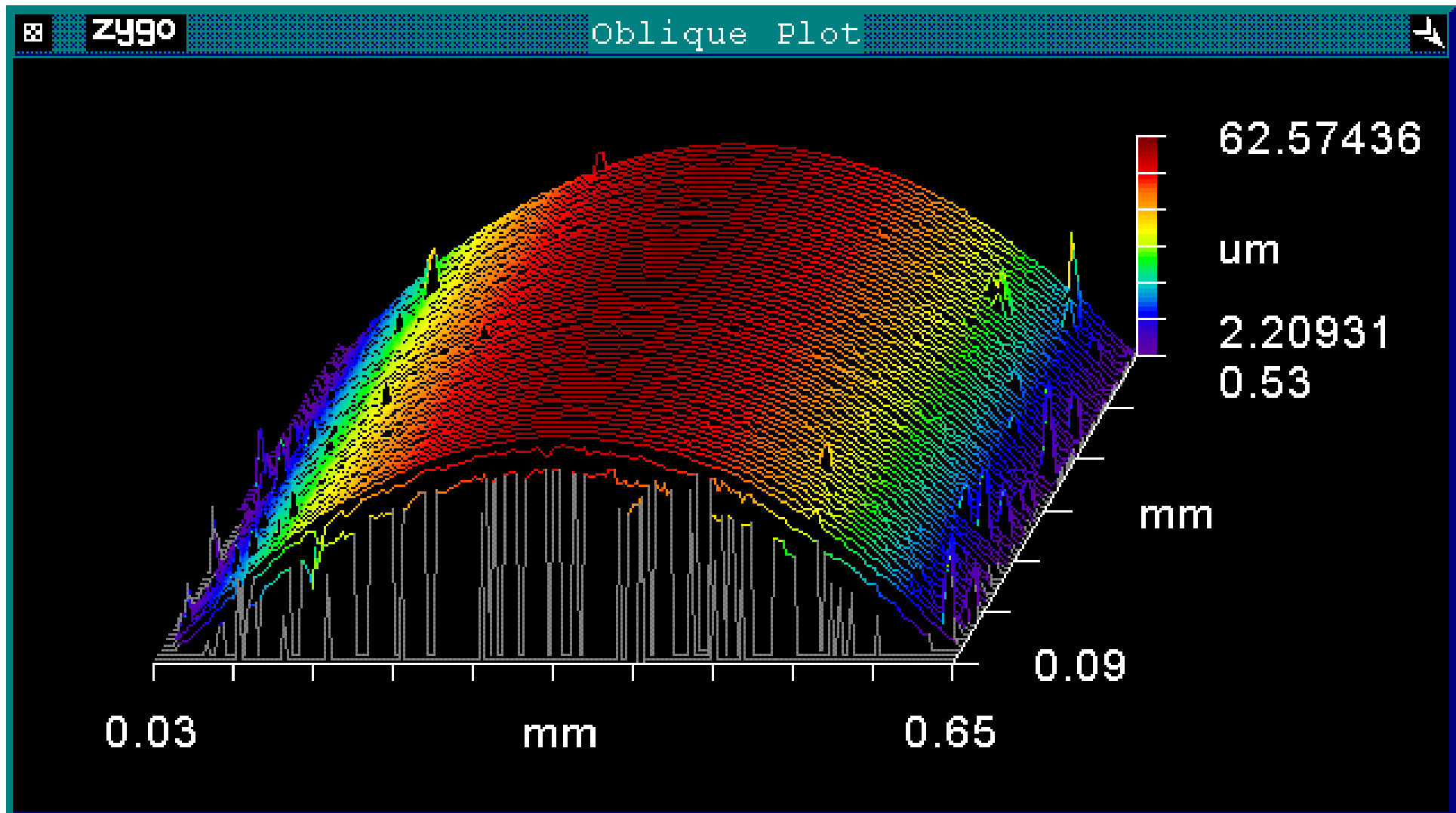
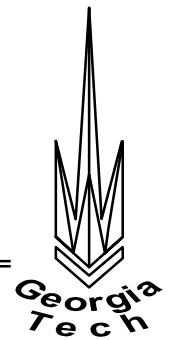
Pass 20



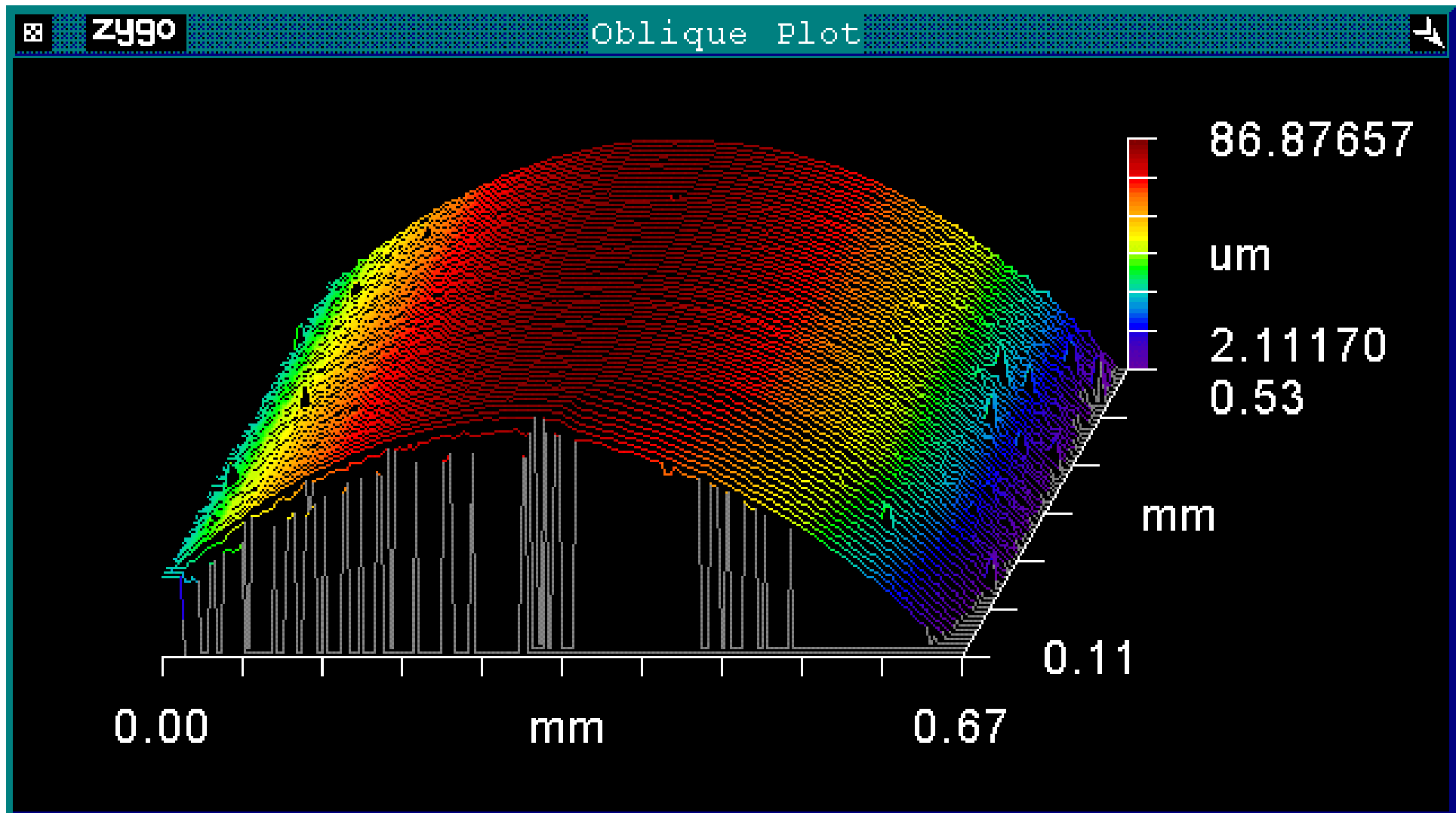
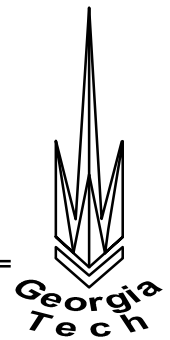
Flank Wear



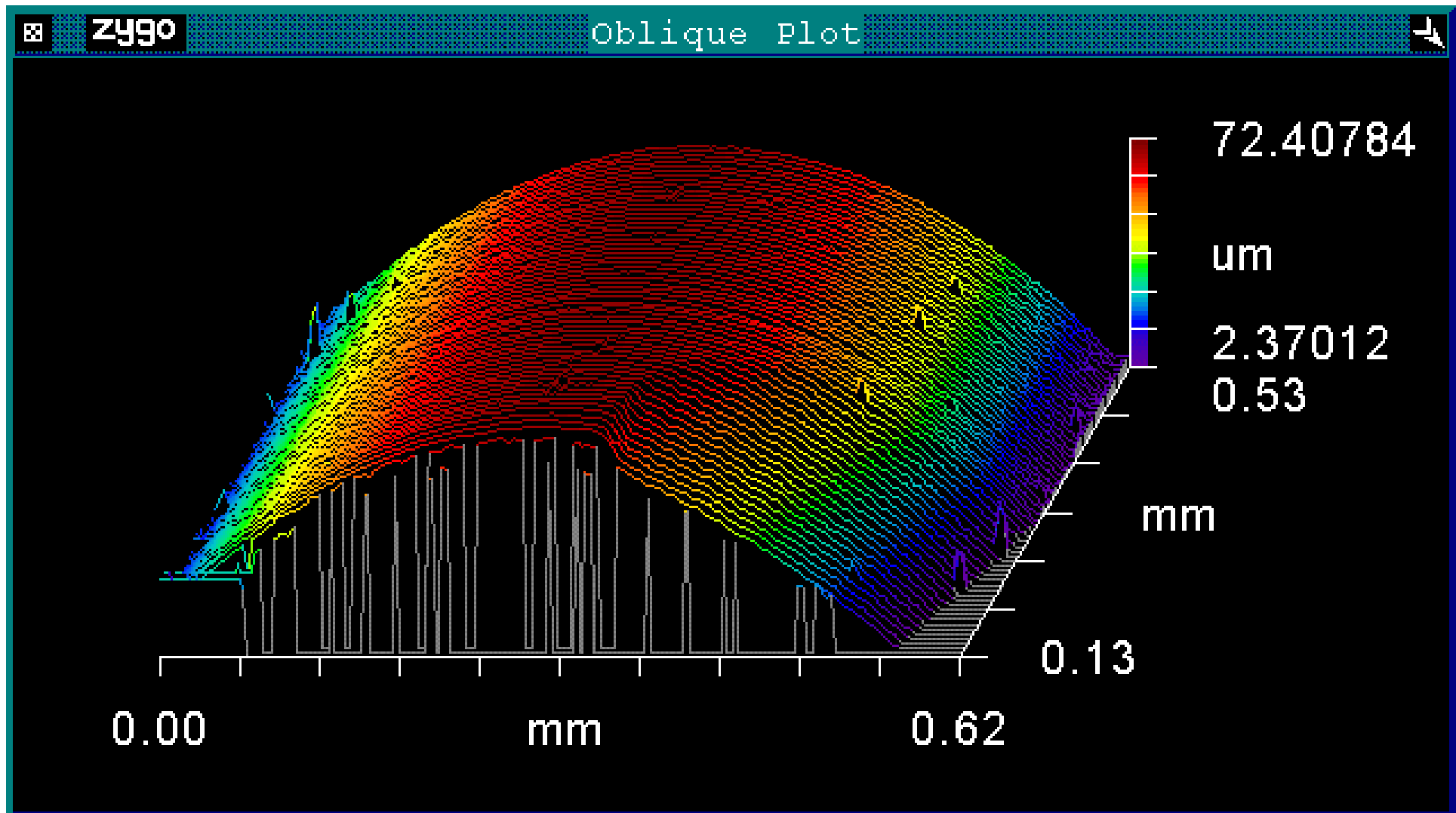
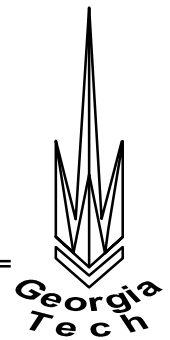
Progression of Flank Wear



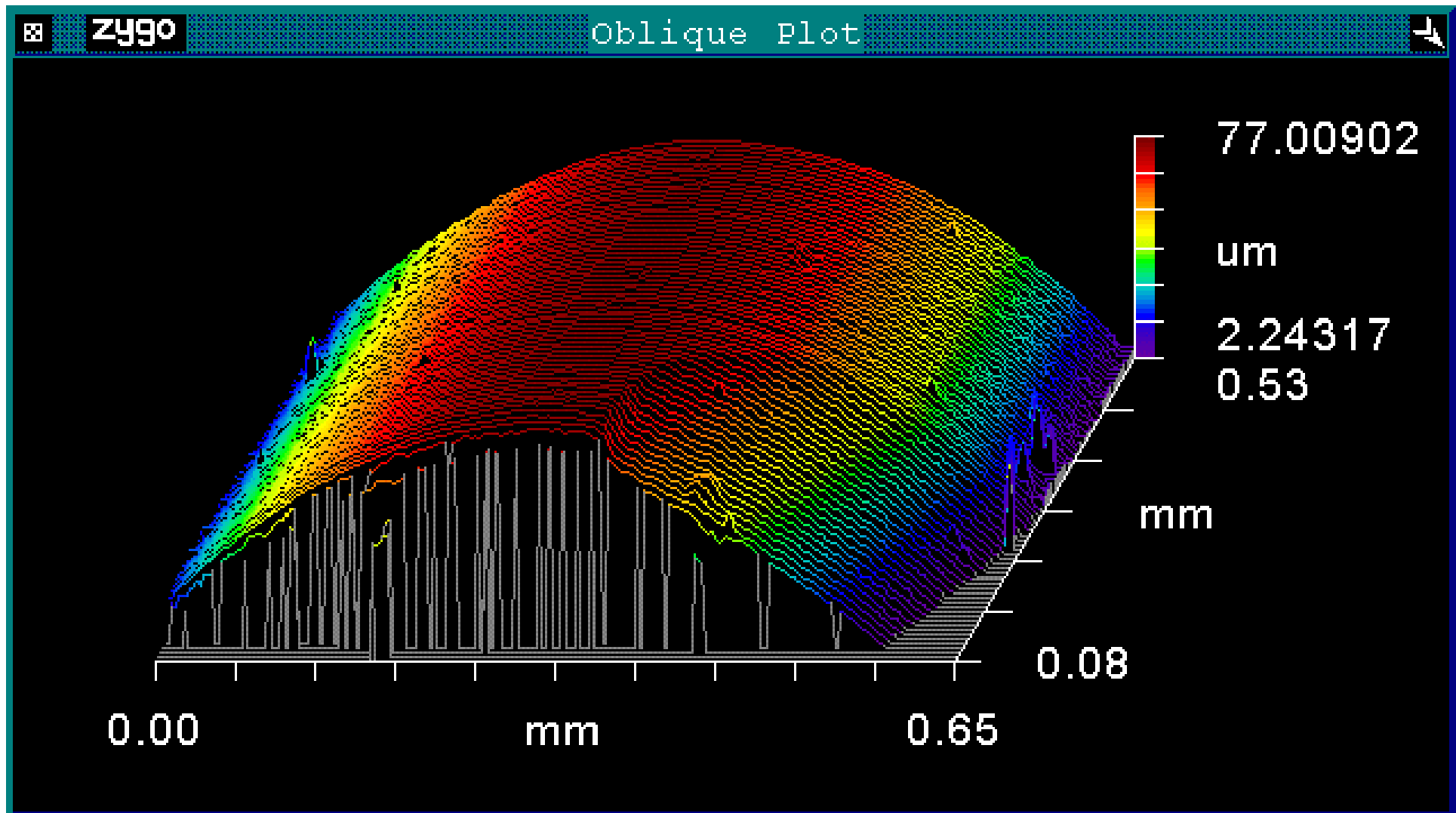
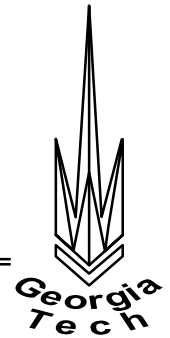
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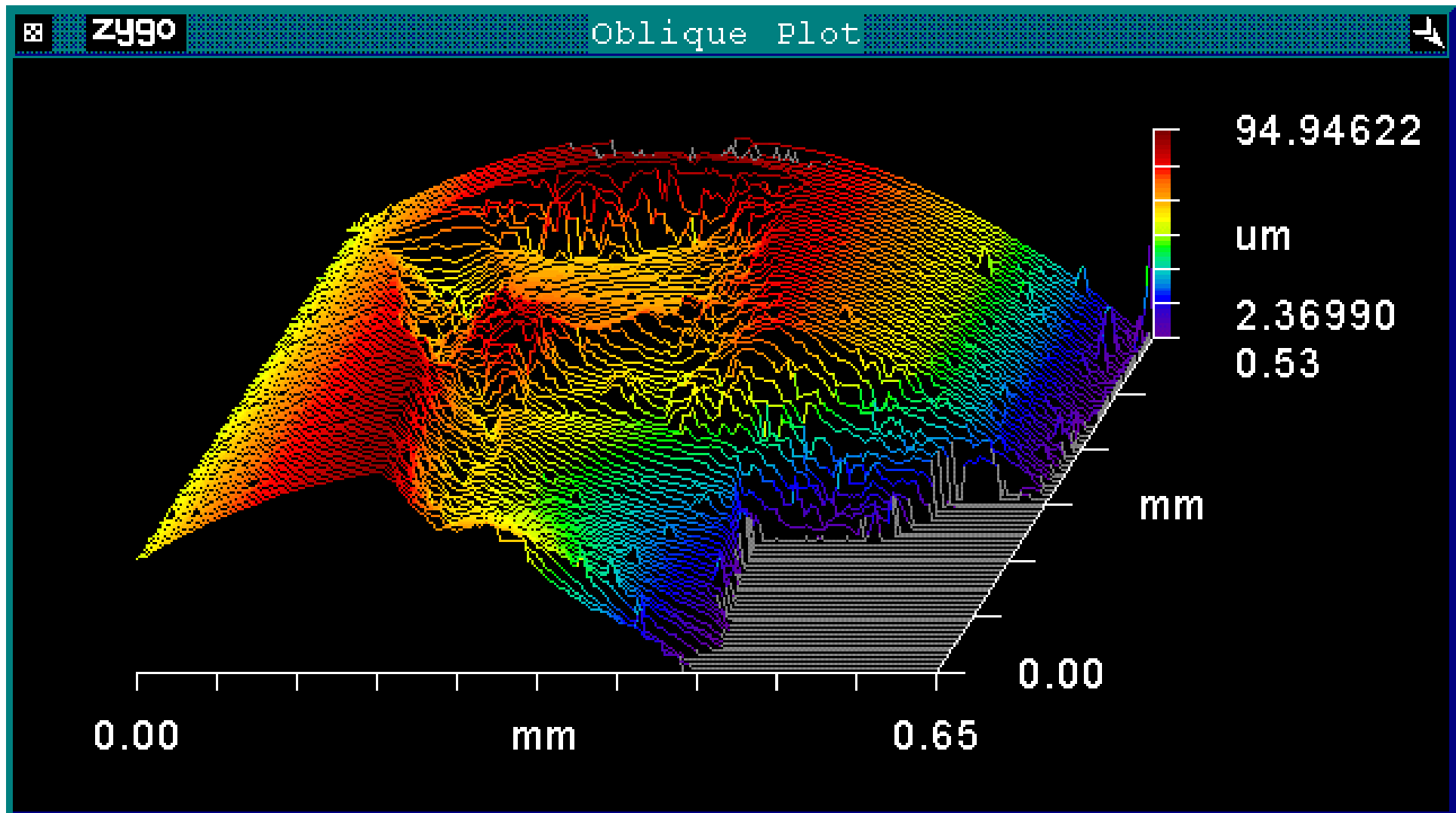
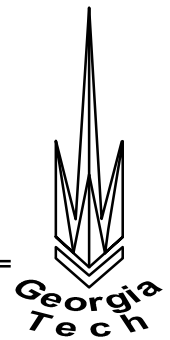
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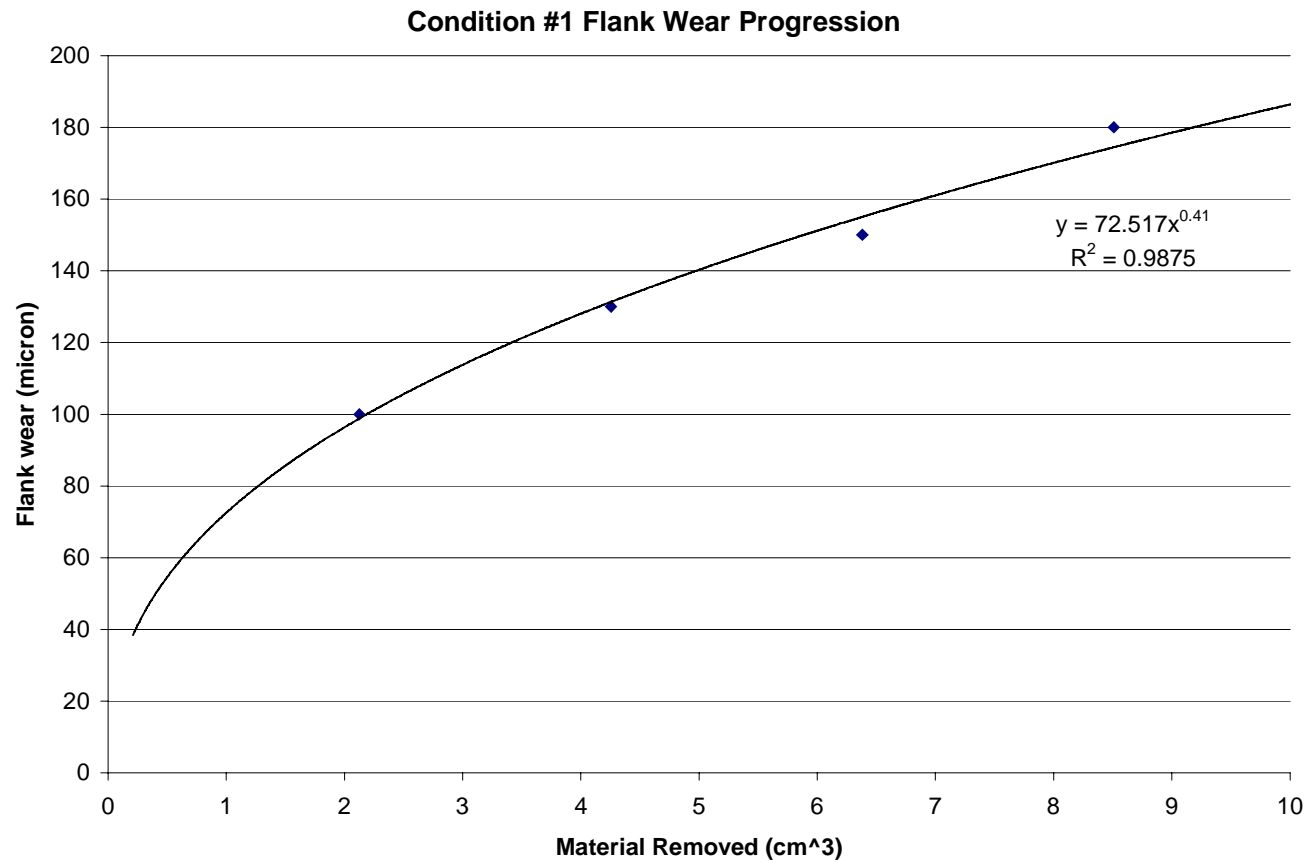
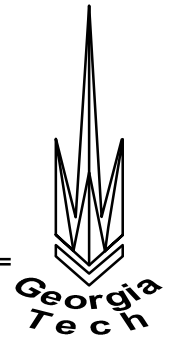
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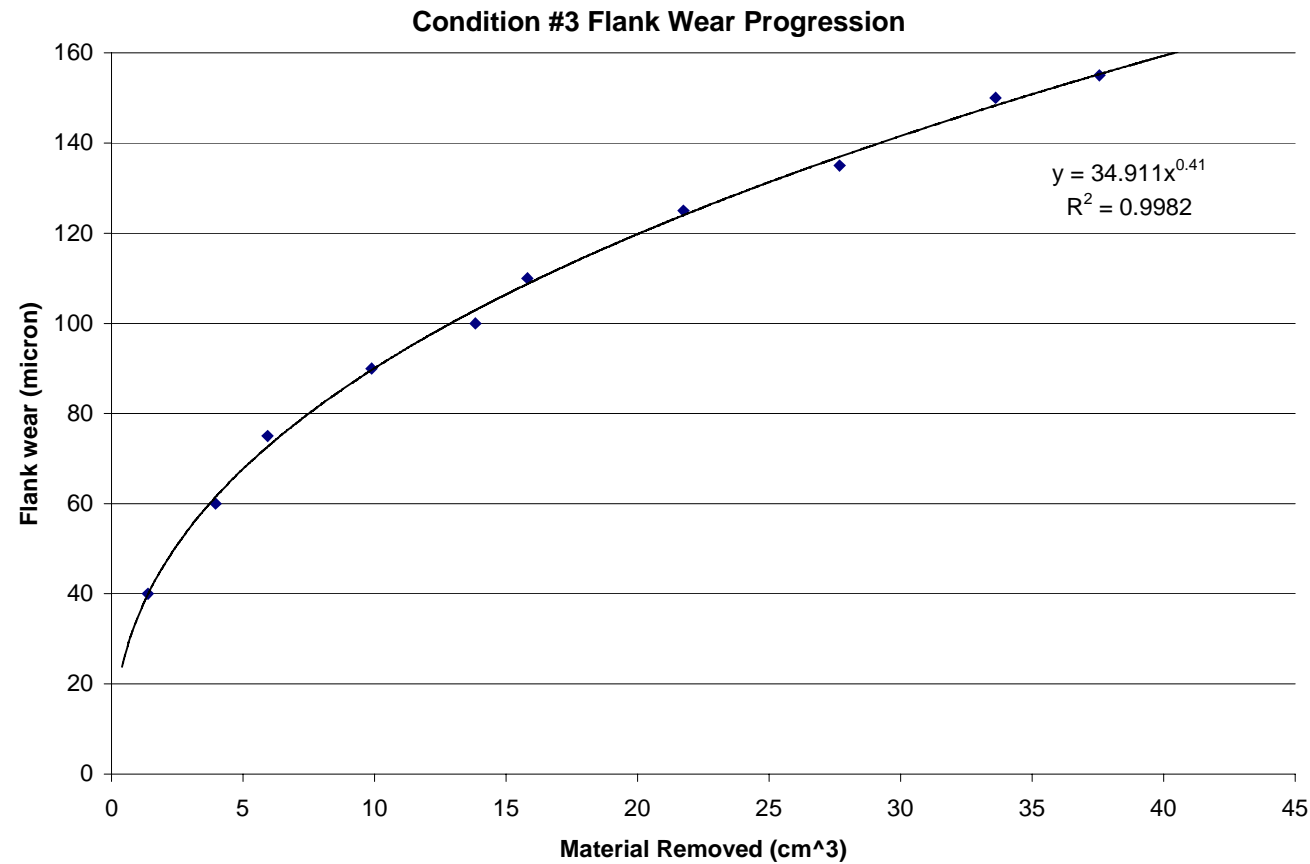
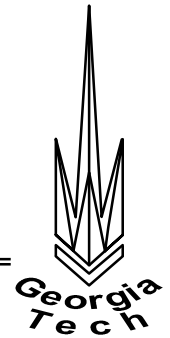
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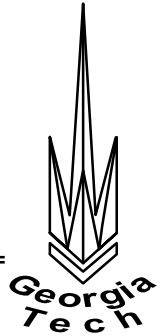
Rate of Flank Wear



Rate of Flank Wear



Conclusions



- The Zygo New View 200 provided a very powerful method for monitoring both crater and flank wear
- Because edge preparation is known to affect cutting results, a qualitative understanding of changes due to crater wear must be important
- Changes in cutting geometry due to crater wear were shown
- Maximum flank land for all conditions was found to be approximately 150 to 200 microns at failure
- A power-law relationship was found between flank wear and volume of removed material
- The cutting conditions appears to change the coefficient of this equation, which could provided a powerful method for determining tool life